

**UNIVERSITY OF
KWAZULU-NATAL**

University of KwaZulu-Natal

**School of Engineering
Discipline of Electrical, Electronic & Computer Engineering**

**UNIVERSITY EXAMINATIONS 2013
OCTOBER 2013**

**ENEL4TB SELECTED TOPICS IN ELECTRONIC ENGINEERING -
MICROWAVES**

Time allowed: 2 hours

Instructions to Candidates:

1. This paper contains 4 questions
2. This paper has 17 pages excluding the cover page
3. Answer **ANY THREE** questions.
4. All questions carry marks as indicated against them
5. Students may bring and use one A4 sheet of relevant formulae
6. Programmable calculators may be used in this examination if the memory is cleared.

The following materials are provided:

1. Vector Analysis Tables
2. Formulae sheets
3. Smith Charts
4. Linear graph papers

Examiners

Prof. Thomas Afullo (Internal)
Prof. Saurabh Sinha (External)

Question 1 (20 Marks)

- a) In free space, at a distance of 2.5 km from a VHF transmitter, the electric field intensity of the propagating wave at a frequency of 150 MHz, is given by:

$$\vec{E}(z, t) = 10^2 \sin(\omega t - \beta z) \hat{x} \text{ V / m}$$

Determine:

- i) The direction of wave propagation
- ii) The magnetic field intensity, $\vec{H}(z, t)$
- iii) The phase constant β
- iv) The Poynting vector, $\vec{S}_{av} = \frac{1}{2} \text{Re}(\vec{E} \times \vec{H}^*)$
- v) The total power received by a yagi antenna of effective aperture $A_e = 5 \text{ cm}^2$.

(10 marks)

- b) A 15-metre RG-8A coaxial cable of inner conductor diameter $d = 2.26 \text{ mm}$ and outer conductor diameter $D = 7.24 \text{ mm}$ is used as a feeder between an 8-GHz microwave radio and a dish antenna. The dielectric material inside the cable has a dielectric constant of 1.95. If the loss per length is given by:

$$\text{Loss}(dB/m) \cong \frac{8.686}{2\pi d Z_o} \sqrt{\frac{\pi f \mu}{\sigma}}$$

If for the copper conductor, the conductivity, $\sigma = 5.8 \times 10^7 \text{ S/m}$, and the magnetic permeability $\mu = 4\pi \times 10^{-7} \text{ H/m}$, determine:

- i) The characteristic impedance of the coaxial cable, Z_o .
- ii) The total power loss inside the coaxial cable.
- iii) The cut-off frequency for the coaxial cable, thus confirm that only one TEM mode operates at 8 GHz.

(10 marks)

Question 2 (20 Marks)

- a) Design a circular waveguide filled with a lossless dielectric of relative permittivity $\epsilon_r=5.0$. The waveguide must operate at a single dominant mode over a bandwidth of 1.2 GHz. Determine:

- i) The radius of the waveguide
- ii) The cut-off frequency for the dominant mode
- iii) The cut-off frequency for the next lowest mode

(8 marks)

- b) The main field for the dominant TE_{mnp} mode in a rectangular cavity resonator of length a , breadth b , and length d , can be expressed as:

$$H_z = -j2H_{zm} \cos\left(\frac{m\pi x}{a}\right) \cos\left(\frac{n\pi y}{b}\right) \sin\left(\frac{p\pi z}{d}\right)$$
$$E_z = 0$$

- i) Determine the expression for cut-off frequency for the dominant mode
- ii) If $a=8$ cm, $b=6$ cm, and $d=15$ cm, determine the cut-off frequency for the lowest TE and TM modes in the cavity.

(8 marks)

- c) Explain the principle of operation of reverberation chambers. Explain expressions for the lowest usable frequency, and how it relates to the lowest resonant frequency.

(4 marks)

Question 3 (20 Marks)

- a) A reflector antenna operating in the upper UHF (800-MHz) band has a far-field radiation intensity, $U(r, \theta, \phi)$ approximated by:

$$U(r, \theta, \phi) = 20 \cos^6 \theta \sin^4 \phi$$

where r , θ , and ϕ are the normal spherical coordinates.

Determine, for this antenna:

- i) The power density, W/m^2
- ii) The total radiated power, in Watts
- iii) The antenna directivity, in dB
- iv) The antenna gain, if the antenna efficiency is 0.63

(10 Marks)

- b) You are required to design a UHF amplifier operating at 800 MHz. Use a GaAS FET with the following parameters:

$$\begin{aligned} S_{11} &= 0.65 \angle -95^\circ & S_{21} &= 5 \angle 115^\circ \\ S_{12} &= 0.035 \angle 40^\circ & S_{22} &= 0.80 \angle -35^\circ \\ Z_o &= 50 \, \Omega \end{aligned}$$

- i) Determine the amplifier stability using the K- Δ test
- ii) Determine the centres and radii of the stability circles.
- iii) Plot the circles on the Smith chart; hence identify areas of stability.

(10 Marks)

Question 4 (20 Marks)

a) Using a low-pass filter prototype, design an equal-ripple high-pass filter with a cut-off frequency at 9 GHz, an impedance of $75\ \Omega$, and 40 dB attenuation at 6 GHz. The ripple factor is 0.5 dB. Determine:

- i) The minimum order of the filter required
- ii) The values of the prototype filter elements
- iii) The scaled element values
- iv) The actual filter circuit.

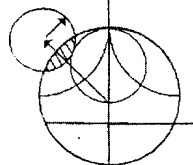
(10 Marks)

b) An rf design engineer is required to design a 3-section Chebyshev transformer to match a $50\text{-}\Omega$ coaxial feeder line to a $120\text{-}\Omega$ antenna. The maximum reflection coefficient allowed, $\Gamma_m=0.015$. Determine:

- i) The reflection coefficient for each section
- ii) The characteristic impedance for each section
- iii) The fractional bandwidth of the designed transformer

(10 Marks)

*****END OF PAPER*****



VECTOR ANALYSIS

Coordinate Transformations

Rectangular to cylindrical:

	x	y	z
ρ	$\cos \phi$	$\sin \phi$	0
ϕ	$-\sin \phi$	$\cos \phi$	0
z	0	0	1

Rectangular to spherical:

	x	y	z
r	$\sin \theta \cos \phi$	$\sin \theta \sin \phi$	$\cos \theta$
θ	$\cos \theta \cos \phi$	$\cos \theta \sin \phi$	$-\sin \theta$
ϕ	$-\sin \phi$	$\cos \phi$	0

Cylindrical to spherical:

	ρ	ϕ	z
r	$\sin \theta$	0	$\cos \theta$
θ	$\cos \theta$	0	$-\sin \theta$
ϕ	0	1	0

These tables can be used to transform unit vectors as well as vector components; e.g.,

$$\hat{\rho} = x \cos \phi + y \sin \phi$$

$$A_{\rho} = A_x \cos \phi + A_y \sin \phi$$

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Vector Differential Operators

Rectangular coordinates:

$$\nabla f = x \frac{\partial f}{\partial x} + y \frac{\partial f}{\partial y} + z \frac{\partial f}{\partial z}$$

$$\nabla \cdot \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z}$$

$$\nabla \times \vec{A} = x \left(\frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} \right) + y \left(\frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} \right) + z \left(\frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} \right)$$

$$\nabla^2 f = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} + \frac{\partial^2 f}{\partial z^2}$$

$$\nabla^2 \vec{A} = x \nabla^2 A_x + y \nabla^2 A_y + z \nabla^2 A_z$$

Cylindrical coordinates:

$$\nabla f = \rho \frac{\partial f}{\partial \rho} + \phi \frac{1}{\rho} \frac{\partial f}{\partial \phi} + z \frac{\partial f}{\partial z}$$

$$\nabla \cdot \vec{A} = \frac{1}{\rho} \frac{\partial}{\partial \rho} (\rho A_{\rho}) + \frac{1}{\rho} \frac{\partial A_{\phi}}{\partial \phi} + \frac{\partial A_z}{\partial z}$$

$$\nabla \times \vec{A} = \rho \left(\frac{1}{\rho} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_{\phi}}{\partial z} \right) + \phi \left(\frac{\partial A_z}{\partial x} - \frac{\partial A_x}{\partial \rho} \right) + z \frac{1}{\rho} \left[\frac{\partial (\rho A_{\phi})}{\partial \rho} - \frac{\partial A_{\rho}}{\partial \phi} \right]$$

$$\nabla^2 f = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho \frac{\partial f}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 f}{\partial \phi^2} + \frac{\partial^2 f}{\partial z^2}$$

$$\nabla^2 \vec{A} = \nabla (\nabla \cdot \vec{A}) - \nabla \times \nabla \times \vec{A}$$

Spherical coordinates:

$$\nabla f = r \frac{\partial f}{\partial r} + \theta \frac{1}{r} \frac{\partial f}{\partial \theta} + \phi \frac{1}{r \sin \theta} \frac{\partial f}{\partial \phi}$$

$$\nabla \cdot \vec{A} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 A_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta A_{\theta}) + \frac{1}{r \sin \theta} \frac{\partial A_{\phi}}{\partial \phi}$$

$$\nabla \times \vec{A} = \frac{\rho}{r \sin \theta} \left[\frac{\partial}{\partial \theta} (A_{\phi} \sin \theta) - \frac{\partial A_{\phi}}{\partial \phi} \right] + \phi \left[\frac{1}{\sin \theta} \frac{\partial A_r}{\partial \phi} - \frac{\partial}{\partial r} (r A_{\phi}) \right] + r \left[\frac{\partial}{\partial r} (r A_{\theta}) - \frac{\partial A_r}{\partial \theta} \right]$$

$$\nabla^2 f = \frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial f}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial f}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 f}{\partial \phi^2}$$

$$\nabla^2 \vec{A} = \nabla \nabla \cdot \vec{A} - \nabla \times \nabla \times \vec{A}$$

Useful mathematical tables

C.1 A brief list of series

$$(1+x)^n = 1 + nx + \frac{n(n-1)}{2!}x^2 + \frac{n(n-1)(n-2)}{3!}x^3 + \cdots |x| < 1$$

$$(1-x)^n = 1 - nx + \frac{n(n-1)}{2!}x^2 - \frac{n(n-1)(n-2)}{3!}x^3 + \cdots |x| < 1$$

$$(1-x)^{-n} = 1 + nx + \frac{n(n+1)}{2!}x^2 + \frac{n(n+1)(n+2)}{3!}x^3 + \cdots |x| < 1$$

$$1 + \frac{1}{2} + \frac{1}{3} + \frac{1}{4} + \cdots = \infty$$

$$1 - \frac{1}{2} + \frac{1}{3} - \frac{1}{4} + \cdots = \ln(2)$$

$$1 - \frac{1}{3} + \frac{1}{5} - \frac{1}{7} + \cdots = \frac{\pi}{4}$$

$$1 + \frac{1}{2^2} + \frac{1}{3^2} + \frac{1}{4^2} + \cdots = \frac{\pi^2}{6}$$

$$1 - \frac{1}{2^2} + \frac{1}{3^2} - \frac{1}{4^2} + \cdots = \frac{\pi^2}{12}$$

$$1 + \frac{1}{3^2} + \frac{1}{5^2} + \frac{1}{7^2} + \cdots = \frac{\pi^2}{8}$$

$$\sin(x) = x - \frac{x^3}{3!} + \frac{x^5}{5!} - \frac{x^7}{7!} + \cdots$$

$$\cos(x) = 1 - \frac{x^2}{2!} + \frac{x^4}{4!} - \frac{x^6}{6!} + \cdots$$

$$\ln(1+x) = \sum_{n=1}^{\infty} (-1)^{n+1} \frac{x^n}{n} \quad \text{for all } x$$

C.2 A list of trigonometric identities

$$e^{\theta} = \cosh(\theta) + \sinh(\theta) = 1 + \theta + \frac{\theta^2}{2!} + \frac{\theta^3}{3!} + \frac{\theta^4}{4!} + \cdots$$

$$e^{j\theta} = \cos(\theta) + j \sin(\theta) \quad \text{where } j = \sqrt{-1}$$

$$\cosh(\theta) = \frac{1}{2}[e^{\theta} + e^{-\theta}]$$

$$\sinh(\theta) = \frac{1}{2}[e^{\theta} - e^{-\theta}]$$

$$\cos(\theta) = \frac{1}{2}[e^{j\theta} + e^{-j\theta}]$$

$$\sin(\theta) = \frac{1}{2j}[e^{j\theta} - e^{-j\theta}]$$

$$\sin(-\alpha) = -\sin(\alpha) \quad \sin(\alpha) = \cos(\alpha - \pi/2)$$

$$\cos(-\alpha) = \cos(\alpha) \quad \cos(\alpha) = -\sin(\alpha - \pi/2)$$

$$\cosh(j\alpha) = \cos(\alpha)$$

$$\sinh(j\alpha) = j \sin(\alpha)$$

$$\cos(j\beta) = \cosh(\beta)$$

$$\sin(j\beta) = j \sinh(\beta)$$

$$\sinh(\alpha + \beta) = \sinh(\alpha) \cosh(\beta) + \cosh(\alpha) \sinh(\beta)$$

$$\cosh(\alpha + \beta) = \cosh(\alpha) \cosh(\beta) + \sinh(\alpha) \sinh(\beta)$$

$$\sinh(\alpha + j\beta) = \sinh(\alpha) \cos(\beta) + j \cosh(\alpha) \sin(\beta)$$

$$\cosh(\alpha + j\beta) = \cosh(\alpha) \cos(\beta) + j \sinh(\alpha) \sin(\beta)$$

$$\sin(\alpha + j\beta) = \sin(\alpha) \cosh(\beta) + j \cos(\alpha) \sinh(\beta)$$

$$\sin(\alpha - j\beta) = \sin(\alpha) \cosh(\beta) - j \cos(\alpha) \sinh(\beta)$$

$$\cos(\alpha + j\beta) = \cos(\alpha) \cosh(\beta) - j \sin(\alpha) \sinh(\beta)$$

$$\cos(\alpha - j\beta) = \cos(\alpha) \cosh(\beta) + j \sin(\alpha) \sinh(\beta)$$

$$\sin(\alpha + \beta) = \sin(\alpha) \cos(\beta) + \cos(\alpha) \sin(\beta)$$

$$\cos(\alpha + \beta) = \cos(\alpha) \cos(\beta) - \sin(\alpha) \sin(\beta)$$

$$\sin(2\alpha) = 2 \sin(\alpha) \cos(\alpha)$$

$$\sin(3\alpha) = 3 \sin(\alpha) - 4 \sin^3(\alpha)$$

$$\cos(2\alpha) = \cos^2(\alpha) - \sin^2(\alpha)$$

$$= 2 \cos^2(\alpha) - 1$$

$$= 1 - 2 \sin^2(\alpha)$$

$$\cos(3\alpha) = 4 \cos^3(\alpha) - 3 \cos(\alpha)$$

$$\sin^2(\alpha) + \cos^2(\alpha) = 1$$

$$1 + \tan^2(\alpha) = \sec^2(\alpha) \quad 1 + \cot^2(\alpha) = \csc^2(\alpha)$$

$$\sin^2(\alpha) = \frac{1}{2}(1 - \cos(2\alpha))$$

$$\cos^2(\alpha) = \frac{1}{2}(1 + \cos(2\alpha))$$

$$\sin^3(\alpha) = \frac{1}{4}(3 \sin(\alpha) - \sin(3\alpha))$$

$$\cos^3(\alpha) = \frac{1}{4}(3 \cos(\alpha) + \cos(3\alpha))$$

$$2 \sin(\alpha) \cos(\beta) = \sin(\alpha + \beta) + \sin(\alpha - \beta)$$

$$2 \cos(\alpha) \cos(\beta) = \cos(\alpha + \beta) + \cos(\alpha - \beta)$$

$$2 \sin(\alpha) \sin(\beta) = \cos(\alpha - \beta) - \cos(\alpha + \beta)$$

$$\tan(\alpha + \beta) = \frac{\tan(\alpha) + \tan(\beta)}{1 - \tan(\alpha) \tan(\beta)}$$

C.3 A list of indefinite integrals

In the list of integrals that follows, C is simply a constant of integration.

$$\text{Let } X = \sqrt{a^2 + x^2}$$

$$\int x^{1/2} dx = \frac{2}{3} x^{3/2} + C$$

$$\int \frac{dx}{\sqrt{x}} = 2\sqrt{x} + C$$

$$\int X dx = \frac{1}{2} x X + \frac{a^2}{2} \ln|x + X| + C$$

$$\int x X dx = \frac{1}{3} X^3 + C$$

$$\int \frac{dx}{X} = \ln|x + X| + C$$

$$\int \frac{dx}{X^3} = \frac{1}{a^2} \frac{x}{X} + C$$

$$\int \frac{dx}{X^5} = \frac{1}{a^4} \left[\frac{x}{X} - \frac{1}{3} \frac{x^3}{X^3} \right] + C$$

$$\int \frac{x dx}{X} = X + C$$

$$\int \frac{x dx}{X^3} = -\frac{1}{X} + C$$

$$\int \frac{x dx}{X^5} = -\frac{1}{3X^3} + C$$

$$\int \frac{dx}{a^2 + x^2} = \frac{1}{a} \tan^{-1}(x/a) + C$$

$$\int \frac{dx}{(a^2 + x^2)^2} = \frac{x}{2a^2(a^2 + x^2)} + \frac{1}{2a^3} \tan^{-1}(x/a) + C$$

$$\int \frac{x dx}{a^2 + x^2} = \frac{1}{2} \ln|a^2 + x^2| + C$$

$$\int \frac{x dx}{(a^2 + x^2)^2} = -\frac{1}{2(a^2 + x^2)} + C$$

$$\int \frac{dx}{a^2 - x^2} = \frac{1}{2a} \ln|(a+x)/(a-x)| + C = \frac{1}{a} \tanh^{-1}(x/a) + C$$

$$\int \frac{x dx}{(a^2 - x^2)} = -\frac{1}{2} \ln|a^2 - x^2| + C$$

$$\int \sin(ax) dx = -\frac{1}{a} \cos(ax) + C$$

$$\int \cos(ax) dx = \frac{1}{a} \sin(ax) + C$$

$$\int \sin^2(ax) dx = \frac{x}{2} - \frac{\sin(2ax)}{4a} + C$$

Appendix C Useful mathematical tables

$$\begin{aligned}
\int \cos^2(ax) \, dx &= \frac{x}{2} + \frac{\sin(2ax)}{4a} + C \\
\int \sin(ax) \cos(bx) \, dx &= -\frac{\cos(a+b)x}{2(a+b)} - \frac{\cos(a-b)x}{2(a-b)}, \quad a \neq \pm b \\
\int \sin(ax) \sin(bx) \, dx &= \frac{\sin(a-b)x}{2(a-b)} - \frac{\sin(a+b)x}{2(a+b)}, \quad a \neq \pm b \\
\int \cos(ax) \cos(bx) \, dx &= \frac{\sin(a-b)x}{2(a-b)} + \frac{\sin(a+b)x}{2(a+b)}, \quad a \neq \pm b \\
\int \sin(ax) \cos(ax) \, dx &= -\frac{\cos(2ax)}{4a} + C \\
\int \sin^n(ax) \cos(ax) \, dx &= \frac{\sin^{n+1}(ax)}{(n+1)a} + C, \quad n \neq -1 \\
\int \tan(ax) \, dx &= -\frac{1}{a} \ln|\cos(ax)| + C \\
\int \cot(ax) \, dx &= \frac{1}{a} \ln|\sin(ax)| + C \\
\int x \sin(ax) \, dx &= \frac{1}{a^2} \sin(ax) - \frac{x}{a} \cos(ax) + C \\
\int x \cos(ax) \, dx &= \frac{1}{a^2} \cos(ax) + \frac{x}{a} \sin(ax) + C \\
\int \tan^2(ax) \, dx &= \frac{1}{a} \tan(ax) - x + C \\
\int \cot^2(ax) \, dx &= -\frac{1}{a} \cot(ax) - x + C \\
\int e^{ax} \, dx &= \frac{1}{a} e^{ax} + C \\
\int b^{ax} \, dx &= \frac{1}{a \ln(b)} b^{ax} + C \\
\int x e^{ax} \, dx &= \frac{e^{ax}}{a^2} (ax - 1) + C \\
\int x^n e^{ax} \, dx &= \frac{1}{a} x^n e^{ax} - \frac{n}{a} \int x^{n-1} e^{ax} \, dx \\
\int e^{ax} \sin(bx) \, dx &= \frac{e^{ax}}{a^2 + b^2} [a \sin(bx) - b \cos(bx)] + C \\
\int e^{ax} \cos(bx) \, dx &= \frac{e^{ax}}{a^2 + b^2} [a \cos(bx) + b \sin(bx)] + C \\
\int \ln(ax) \, dx &= x \ln(ax) - x + C \\
\int x^n \ln(ax) \, dx &= \frac{x^{n+1}}{n+1} \ln(ax) - \frac{x^{n+1}}{(n+1)^2} + C \quad n \neq -1 \\
\int \frac{1}{x} \ln(ax) \, dx &= \frac{1}{2} [\ln(ax)]^2 + C \\
\int \sinh(ax) \, dx &= \frac{1}{a} \cosh(ax) + C
\end{aligned}$$

$$\begin{aligned}
\int \cosh(ax) \, dx &= \frac{1}{a} \sinh(ax) + C \\
\int \tanh(ax) \, dx &= \frac{1}{a} \ln[\cosh(ax)] + C \\
\int \coth(ax) \, dx &= \frac{1}{a} \ln|\sinh(ax)| + C \\
\int \operatorname{sech}(ax) \, dx &= \frac{1}{a} \sin^{-1}[\tanh(ax)] + C \\
\int \operatorname{csch}(ax) \, dx &= \frac{1}{a} \ln|\tanh(ax/2)| + C \\
\int \sinh^2(ax) \, dx &= \frac{\sinh(2ax)}{4a} - \frac{x}{2} + C \\
\int \cosh^2(ax) \, dx &= \frac{\sinh(2ax)}{4a} + \frac{x}{2} + C \\
\int \tanh^2(ax) \, dx &= x - \frac{1}{a} \tanh(ax) + C \\
\int \coth^2(ax) \, dx &= x - \frac{1}{a} \coth(ax) + C \\
\int \operatorname{sech}^2(ax) \, dx &= \frac{1}{a} \tanh(ax) + C \\
\int \operatorname{csch}^2(ax) \, dx &= -\frac{1}{a} \coth(ax) + C
\end{aligned}$$

C.4 A partial list of definite integrals

$$\begin{aligned}
\int_0^\infty e^{-ax} \, dx &= \frac{1}{a} \quad (a > 0) \\
\int_0^\infty x e^{-ax} \, dx &= \frac{1}{a^2} \quad (a > 0) \\
\int_0^\infty x^2 e^{-ax} \, dx &= \frac{2}{a^3} \quad (a > 0) \\
\int_0^\infty x^n e^{-ax} \, dx &= \frac{n!}{a^{n+1}} \quad (a > 0, n > -1) \\
\int_0^\infty x^{1/2} e^{-ax} \, dx &= \frac{1}{2a} \sqrt{\pi/a} \quad (a > 0) \\
\int_0^\infty x^{-1/2} e^{-ax} \, dx &= \sqrt{\pi/a} \quad (a > 0) \\
\int_0^\infty e^{-ax} \sin(bx) \, dx &= \frac{b}{a^2 + b^2} \quad (a > 0) \\
\int_0^\infty e^{-ax} \cos(bx) \, dx &= \frac{a}{a^2 + b^2} \quad (a > 0) \\
\int_0^\infty x e^{-ax} \sin(bx) \, dx &= \frac{2ab}{(a^2 + b^2)^2} \quad (a > 0)
\end{aligned}$$

Appendix C Useful mathematical tables

$$\int_0^{\infty} x e^{-ax} \cos(bx) dx = \frac{a^2 - b^2}{(a^2 + b^2)^2} \quad (a > 0)$$

$$\int_0^{2\pi} \sin(ax) dx = 0 \quad (a = 1, 2, 3, \dots)$$

$$\int_0^{2\pi} \cos(ax) dx = 0 \quad (a = 1, 2, 3, \dots)$$

$$\int_0^{2\pi} \sin^2(ax) dx = \pi \quad (a = 1, 2, 3, \dots)$$

$$\int_0^{2\pi} \cos^2(ax) dx = \pi \quad (a = 1, 2, 3, \dots)$$

$$\int_0^{\pi} \cos(ax) dx = 0 \quad (a = 1, 2, 3, \dots)$$

$$\int_0^{\pi} \sin(ax) dx = \frac{1}{a} [1 - \cos(a\pi)] \quad (a = 1, 2, 3, \dots)$$

$$\int_0^{\pi} \sin^2(ax) dx = \frac{\pi}{2} \quad (a = 1, 2, 3, \dots)$$

$$\int_0^{\pi} \cos^2(ax) dx = \frac{\pi}{2} \quad (a = 1, 2, 3, \dots)$$

$$\int_0^{\pi} \sin(ax) \sin(bx) dx = 0 \quad a \neq b \text{ (} a \text{ and } b \text{ are integers)}$$

$$\int_0^{\pi} \cos(ax) \cos(bx) dx = 0 \quad a \neq b \text{ (} a \text{ and } b \text{ are integers)}$$

$$\int_0^{\pi} \sin(ax) \cos(bx) dx = 0 \quad a = b \text{ (} a \text{ and } b \text{ are integers)}$$

$$= 0 \quad a \neq b \text{ but } (a + b) \text{ even}$$

$$= \frac{2a}{a^2 - b^2} \quad a \neq b \text{ but } (a + b) \text{ odd}$$

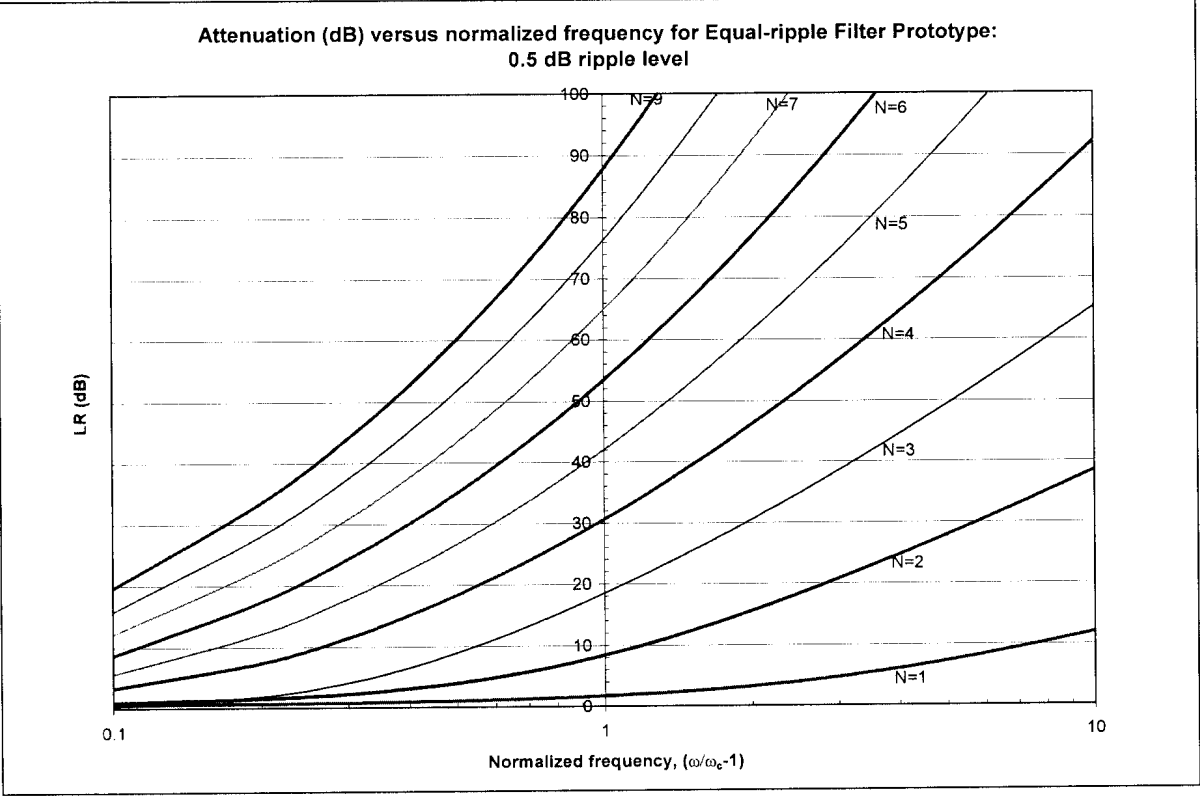
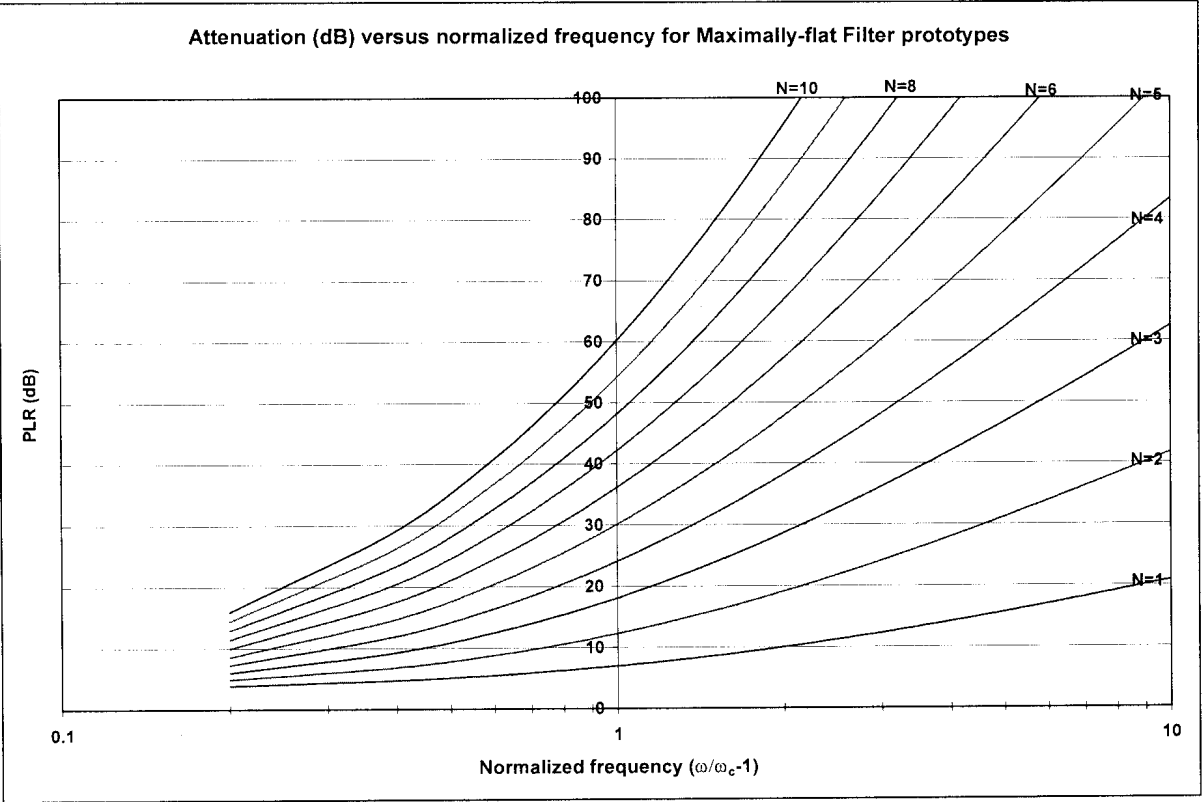
$$\int_0^{\pi/2} \sin(ax) dx = \frac{1}{a} [1 - \cos(a\pi/2)]$$

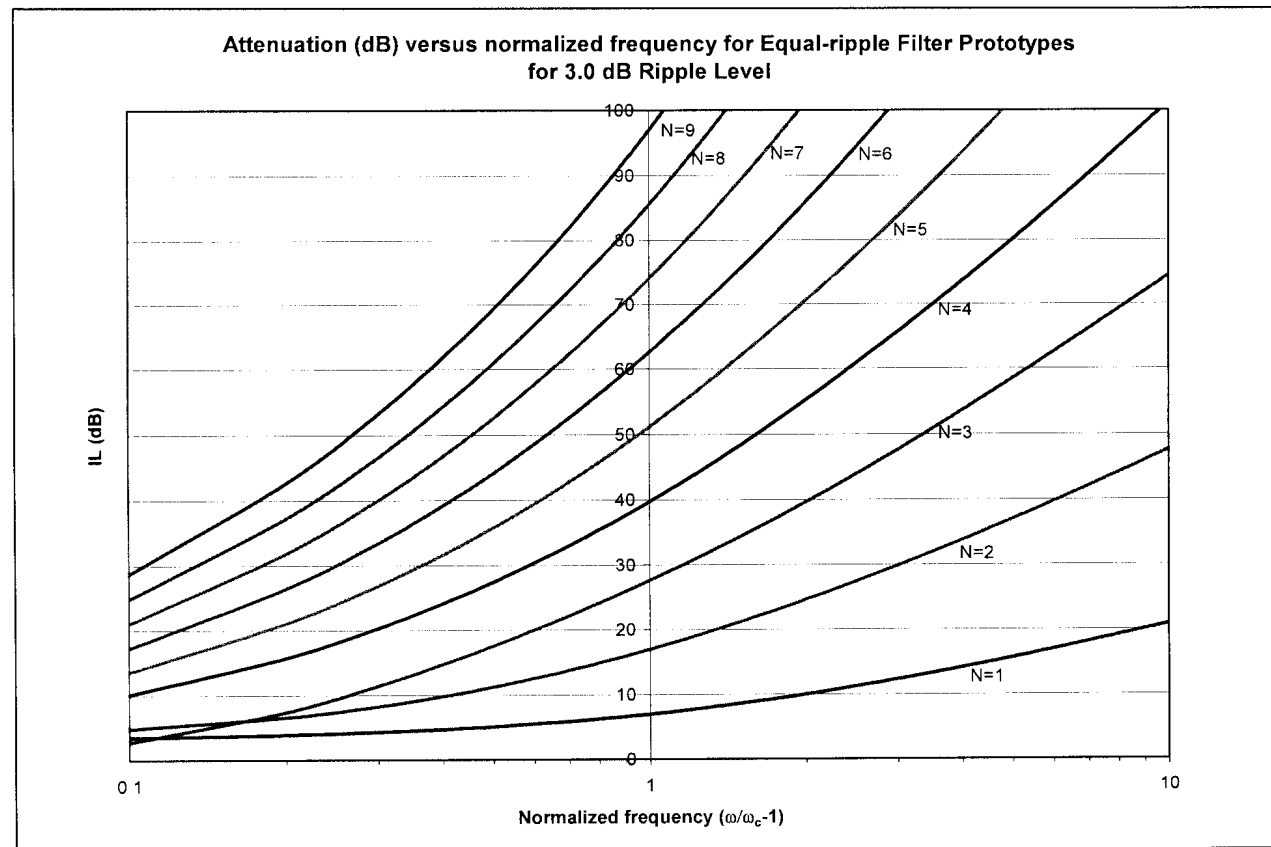
$$\int_0^{\pi/2} \cos(ax) dx = \frac{1}{a} \sin(a\pi/2)$$

$$\int_0^{\pi/2} \sin^2(ax) dx = \frac{\pi}{4} \quad (a = 1, 2, 3, \dots)$$

$$\int_0^{\pi/2} \cos^2(ax) dx = \frac{\pi}{4} \quad (a = 1, 2, 3, \dots)$$

APPENDIX 2: MAXIMALLY FLAT & EQUAL-RIPPLE FILTER PLOTS AND TABLE





n	$n - th$ order Butterworth Polynomial
1	$(s + 1)$
2	$(s^2 + \sqrt{2}s + 1)$
3	$(s + 1)(s^2 + s + 1)$
4	$(s^2 + 0.765s + 1)(s^2 + 1.848s + 1)$
5	$(s + 1)(s^2 + 0.618s + 1)(s^2 + 1.618s + 1)$
6	$(s^2 + 0.518s + 1)(s^2 + \sqrt{2}s + 1)(s^2 + 1.932s + 1)$
7	$(s + 1)(s^2 + 0.445s + 1)(s^2 + 1.247s + 1)(s^2 + 1.802s + 1)$
8	$(s^2 + 0.390s + 1)(s^2 + 1.111s + 1)(s^2 + 1.6663s + 1)(s^2 + 1.962s + 1)$

N	g_1	g_2	g_3	g_4	g_5	g_6	g_7	g_8	g_9	g_{10}	g_{11}
1	2.0000	1.0000									
2	1.4142	1.4142	1.0000								
3	1.0000	2.0000	1.0000	1.0000							
4	0.7654	1.8478	1.8478	0.7654	1.0000						
5	0.6180	1.6180	2.0000	1.6180	0.6180	1.0000					
6	0.5176	1.4142	1.9318	1.9318	1.4142	0.5176	1.0000				
7	0.4450	1.2470	1.8019	2.0000	1.8019	1.2470	0.4450	1.0000			
8	0.3902	1.1111	1.6629	1.9615	1.9615	1.6629	1.1111	0.3902	1.0000		
9	0.3473	1.0000	1.5321	1.8794	2.0000	1.8794	1.5321	1.0000	0.3473	1.0000	
10	0.3129	0.9080	1.4142	1.7820	1.9754	1.9754	1.7820	1.4142	0.9080	0.3129	1.0000

ELEMENT VALUES FOR MAXIMALLY FLAT LOW-PASS FILTER PROTOTYPES ($g_0=1$, $\omega_c=1$, $N=1$ to 10)

N	g_1	g_2	g_3	g_4	g_5	g_6	g_7	g_8	g_9	g_{10}	g_{11}
1	0.6986	1.0000									
2	1.4029	0.7071	1.9841								
3	1.5963	1.0967	1.5963	1.0000							
4	1.6703	1.1926	2.3661	0.8419	1.9841						
5	1.7058	1.2296	2.5408	1.2296	1.7058	1.0000					
6	1.7254	1.2479	2.6064	1.3137	2.4758	0.8696	1.9841				
7	1.7372	1.2583	2.6381	1.3444	2.6381	1.2583	1.7372	1.0000			
8	1.7451	1.2647	2.6564	1.3590	2.6964	1.3389	2.5093	0.8796	1.9841		
9	1.7504	1.2690	2.6678	1.3673	2.7239	1.3673	2.6678	1.2690	1.7504	1.0000	
10	1.7543	1.2721	2.6754	1.3725	2.7392	1.3806	2.7231	1.3485	2.5239	0.8842	1.9841

ELEMENT VALUES FOR EQUAL-RIPPLE LOW-PASS FILTER PROTOTYPES ($g_0=1$, $\omega_c=1$, $N=1$ to 10) – 0.5 dB Ripple

N	g_1	g_2	g_3	g_4	g_5	g_6	g_7	g_8	g_9	g_{10}	g_{11}
1	1.9953	1.0000									
2	3.1013	0.5339	5.8095								
3	3.3487	0.7117	3.3487	1.0000							
4	3.4389	0.7483	4.3471	0.5920	5.8095						
5	3.4817	0.7618	4.5381	0.7618	3.4817	1.0000					
6	3.5045	0.7685	4.6061	0.7929	4.4641	0.6033	5.8095				
7	3.5182	0.7723	4.6386	0.8039	4.6386	0.7723	3.5182	1.0000			
8	3.5277	0.7745	4.6575	0.8089	4.6990	0.8018	4.4990	0.6073	5.8095		
9	3.5340	0.7760	4.6692	0.8118	4.7272	0.8118	4.6692	0.7760	3.5340	1.0000	
10	3.5384	0.7771	4.6768	0.8136	4.7425	0.8164	4.7260	0.8051	4.5142	0.6091	5.8095

ELEMENT VALUES FOR EQUAL-RIPPLE LOW-PASS FILTER PROTOTYPES ($g_0=1$, $\omega_c=1$, $N=1$ to 10) – 3.0 dB Ripple

APPENDIX 3: MICROWAVE AMPLIFIER DESIGN FORMULAE

i) The K-Δ Test for Stability

$$|\Delta| = |s_{11}s_{22} - s_{12}s_{21}| < 1$$

$$|K| = \left| \frac{1 - |s_{11}|^2 - |s_{22}|^2 + \Delta^2}{2|s_{21}s_{12}|} \right| > 1$$

ii) The μ Test for Stability:

$$\mu = \frac{1 - |s_{11}|^2}{|s_{22} - \Delta s_{11}^*| + |s_{12}s_{21}|} > 1$$

iii) Input and Output Reflection Coefficients

$$|\Gamma_{in}| = \left| s_{11} + \frac{s_{12}\Gamma_L s_{21}}{1 - s_{22}\Gamma_L} \right| < 1; \quad |\Gamma_{out}| = \left| s_{22} + \frac{s_{21}\Gamma_g s_{12}}{1 - s_{11}\Gamma_g} \right| < 1$$

$$\Gamma_L = \frac{Z_L - Z_o}{Z_L + Z_o}; \quad \Gamma_g = \frac{Z_g - Z_o}{Z_g + Z_o}$$

iv) Load (output) and source (input) stability circles with centre C_L and radius R_L :

$$C_L = \frac{(s_{22} - \Delta s_{11}^*)^*}{|s_{22}|^2 - |\Delta|^2} \quad R_L = \left| \frac{s_{12}s_{21}}{|s_{22}|^2 - |\Delta|^2} \right|$$

$$C_g = \frac{(s_{11} - \Delta s_{22}^*)^*}{|s_{11}|^2 - |\Delta|^2} \quad R_g = \left| \frac{s_{12}s_{21}}{|s_{11}|^2 - |\Delta|^2} \right|$$

v) Conjugate Matching for Maximum Gain, G_T

$$\begin{aligned}
\Gamma_{gM} &= \frac{B_1 - \sqrt{B_1^2 - 4|C_1|^2}}{2C_1} & \Gamma_{LM} &= \frac{B_2 - \sqrt{B_2^2 - 4|C_2|^2}}{2C_2} \\
B_1 &= 1 + |S_{11}|^2 - |S_{22}|^2 - |\Delta|^2 & B_2 &= 1 + |S_{22}|^2 - |S_{11}|^2 - |\Delta|^2 \\
C_1 &= S_{11} - \Delta S_{22}^* & C_2 &= S_{22} - \Delta S_{11}^* \\
G_T &= G_g G_o G_L & G_o &= |S_{21}|^2 \\
G_g &= \frac{1}{1 - |\Gamma_{gM}|^2} & G_L &= \frac{1 - |\Gamma_{LM}|^2}{|1 - S_{22}\Gamma_{LM}|^2}
\end{aligned}$$

APPENDIX 4: QUARTER-WAVE TRANSFORMER DESIGN FORMULAE

i) The reflection coefficient at the n-th section is:

$$\Gamma_n = \frac{Z_{n+1} - Z_n}{Z_{n+1} + Z_n}$$

ii) Defining Γ_m , as maximum reflection coefficient that can be tolerated:

$$\begin{aligned}
\frac{1}{\Gamma_m^2} &= 1 + \left(\frac{2\sqrt{Z_o Z_L}}{Z_L - Z_o} \sec \theta_m \right)^2 \\
\cos \theta_m &= \frac{\Gamma_m}{\sqrt{1 - \Gamma_m^2}} \left(\frac{2\sqrt{Z_o Z_L}}{|Z_L - Z_o|} \right)
\end{aligned}$$

iii) The fractional bandwidth is:

$$\frac{\Delta f}{f_o} = \frac{2(f_o - f_m)}{f_o} = 2 - \frac{2f_m}{f_o} = 2 - \frac{4\theta_m}{\pi} = 2 - \frac{4}{\pi} \cos^{-1} \left[\frac{\Gamma_m}{\sqrt{1 - \Gamma_m^2}} \frac{2\sqrt{Z_o Z_L}}{|Z_L - Z_o|} \right]$$

iv) The first four polynomials for the Chebyshev transformer design are:

$$T_1(x) = x; \quad T_2(x) = 2x^2 - 1$$

$$T_3(x) = 4x^3 - 3x; \quad T_4(x) = 8x^4 - 8x^2 + 1$$

APPENDIX 5: WAVEGUIDE PARAMETERS

$$\beta_{g,mn} = \frac{\omega}{v_p} \sqrt{1 - \frac{f_{c,mn}^2}{f^2}} = \beta \sqrt{1 - \frac{f_{c,mn}^2}{f^2}}; \quad f_{c,mn} = \frac{1}{2\pi\sqrt{\mu\epsilon}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

$$\eta_{nm}^{TM} = \frac{E_x}{H_y} = -j \frac{\alpha_{g,mn}}{\omega\epsilon}; \quad \eta_{nm}^{TE} = \frac{E_x}{H_y} = -\frac{E_y}{H_x} = \frac{j\omega\mu}{\alpha_{g,mn}}$$

$$v_{p,mn} = \frac{\omega}{\beta_{g,mn}} = \frac{v_p}{\sqrt{1 - \left(\frac{f_{c,mn}}{f}\right)^2}}; \quad v_{g,mn} = \frac{d\omega}{d\beta_{g,mn}} = v_p \sqrt{1 - \left(\frac{f_{c,mn}}{f}\right)^2}$$

$$P_{av} = \frac{\beta_{mn}^2 a^3 b^3}{8(n^2 a^2 + m^2 b^2)} \frac{E_{zm}^2}{\eta_{mn}^{TM}} \quad P_{av} = \eta_{mn}^{TE} \left[\frac{\beta_{mn}^2 a^3 b^3}{8\pi^2 (n^2 a^2 + m^2 b^2)} H_{zm}^2 \right]$$

LOSSES IN A RECTANGULAR WAVEGUIDE

$$\alpha_{10} = \frac{1}{\sigma_c \delta_c \eta b} \left[\frac{1 + \frac{2b}{a} \left(\frac{f}{f_{c,10}}\right)^2}{\sqrt{1 - \left(\frac{f_{c,10}}{f}\right)^2}} \right]$$

BESSEL FUNCTIONS $J_{mn}(k_c a)=0$:						BESSEL FUNCTIONS $J'_{mn}(k_c a)=0$:					
$n \rightarrow$	0	1	2	3	4	$n \rightarrow$	0	1	2	3	4
$m \downarrow$						$m \downarrow$					
1	2.4	3.83	5.14	6.38	7.59	1	3.83	1.84	3.05	4.20	5.32
2	5.52	7.02	8.42	9.76	11.06	2	7.02	5.33	6.71	8.02	9.28
3	8.65	10.17	11.62	13.02	14.37	3	10.17	8.54	9.97	11.35	12.68